THE FUTURE OF STEEL CONSTRUCTION

Eurocode Second Generation Updates EN 1990 Basis of Design and EN 1991 Actions on Structures

Mungo Stacy



30 March 2028

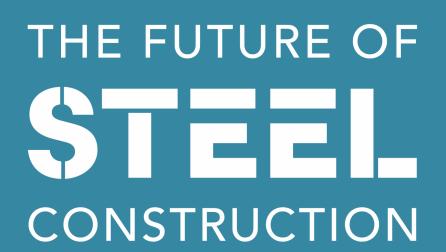
Eurocode Second Generation Updates



Verification of adequacy



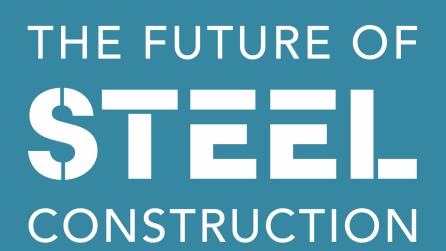
New societal demands



Research to application

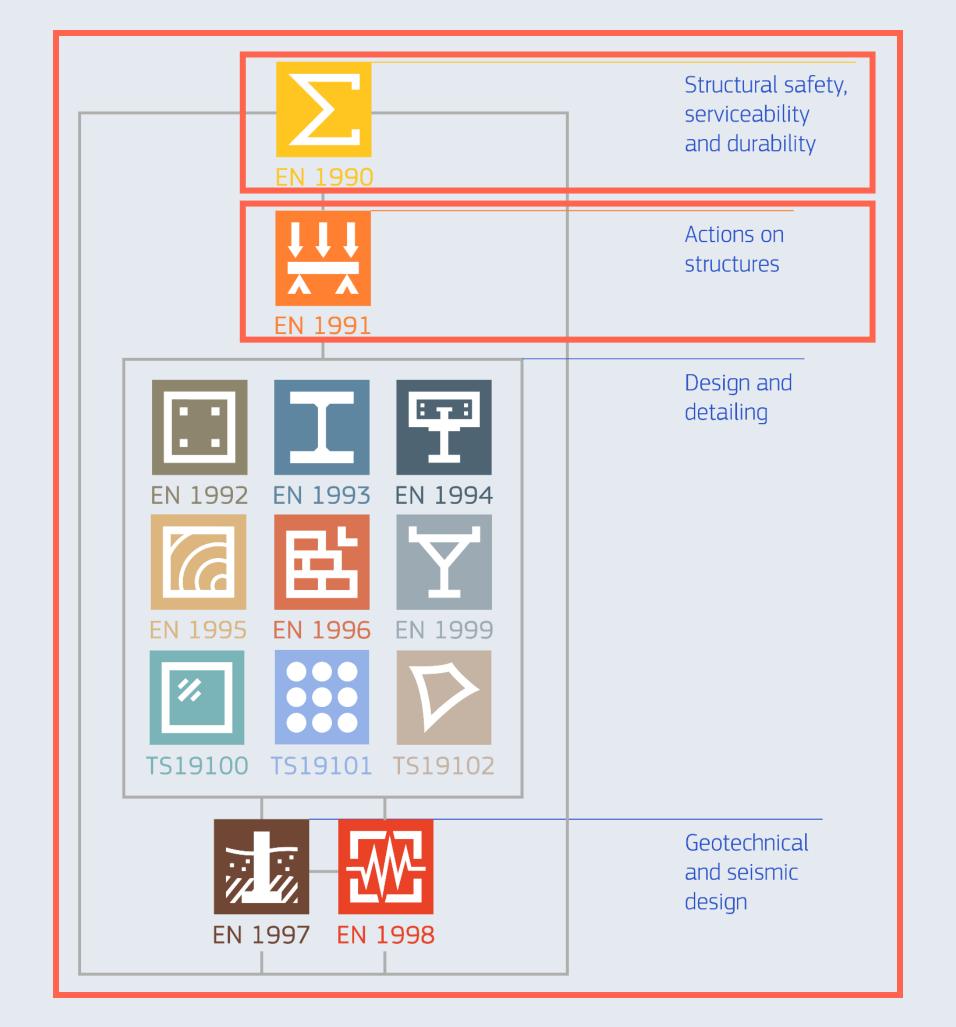


Feedback



Impact

Eurocode Second Generation Updates EN 1990 Basis of Design and EN 1991 Actions on Structures





Aims for the evolution of Structural Eurocodes

✓ Enhanced Ease of Use ✓ Exemplary levels of international consensus



Aims for the evolution of Structural Eurocodes

✓ Enhanced Ease of Use ✓ Exemplary levels of international consensus



Statements of intent to meet our user's needs (1 of 2)

CATEGORIES OF EUROCODES' USERS

Practitioners – Competent engineers [Primary target audience]

Practioners – Graduates

Expert specialists

Product Manufacturers

CEN/TC 250 STATEMENTS OF INTENT

We will aim to produce Standards that are suitable and clear for all common design cases without demanding disproportionate levels of effort to apply them

We will aim to produce Eurocodes that can be used by Graduates where necessary supplemented by suitable guidance documents and textbooks and under the supervision of an experienced practitioner when appropriate

We will aim not to restrict innovation by providing freedom to experts to apply their specialist knowledge and expertise

Working with other CEN/TCs we will aim to eliminate incompatibilities or ambiguities between the Eurocodes and Product Standards



Statements of intent to meet our user's needs (2 of 2)

CATEGORIES OF EUROCODES' USERS

CEN/TC 250 STATEMENTS OF INTENT

Software developers

We will aim to provide unambiguous and complete design procedures.

Accompanying formulae will be provided for charts and tables where possible

Educators

We will aim to use consistent underlying technical principles irrespective of the intended use of a structure (e.g. bridge, building, etc.) and that facilitate the linkage between physical behaviour and design rules

National regulator

We will endeavour to produce standards that can be referenced or quoted by National Regulations

Private sectors businesses

We will continue to promote technical harmonization across European markets in order to reduce barriers to trade

Clients

We will produce Eurocodes that enable the design of safe, serviceable, robust and durable structures, aiming to promoting cost effectiveness throughout their whole life cycle, including design, construction and maintenance

Other CEN/TCs

We will engage proactively to promote effective collaboration with those other CEN/TCs that have shared interests



Principles and priorities

General principles (primary)

- 1 Improving clarity and understandability of technical provisions of the Eurocodes
- 2 Improving accessibility to technical provisions and ease of navigation between them
- 3 Improving consistency within and between the Eurocodes
- Including state-of the-art material the use of which is based on commonly accepted results of research and has been validated through sufficient practical experience
- 5 Considering the second generation of the Eurocodes as an "evolution" avoiding fundamental changes to the approach to design and to the structure of the Eurocodes unless adequately justified

Specific principles (secondary)

- 6 Providing clear guidance for all common design cases encountered by typical competent practitioners in the relevant field
- 7 Omitting or providing only general and basic technical provisions for special cases that will be very rarely encountered by typical competent practitioners in the relevant field
- Not inhibiting the freedom of experts to work from first principles and providing adequate freedom for innovation
- 9 Limiting the inclusion of alternative application rules
- Including simplified methods only where they are of general application, address commonly encountered situations, are technically justified and give more conservative results than the rigorous methods they are intended to simplify
- 11 Improving consistency with product standards and standards for execution
- 12 Providing technical provisions that are not excessive sensitive to execution tolerances beyond what can be practically achieved on site



Aims for the evolution of Structural Eurocodes

✓ Enhanced Ease of Use

✓ Exemplary levels of international consensus



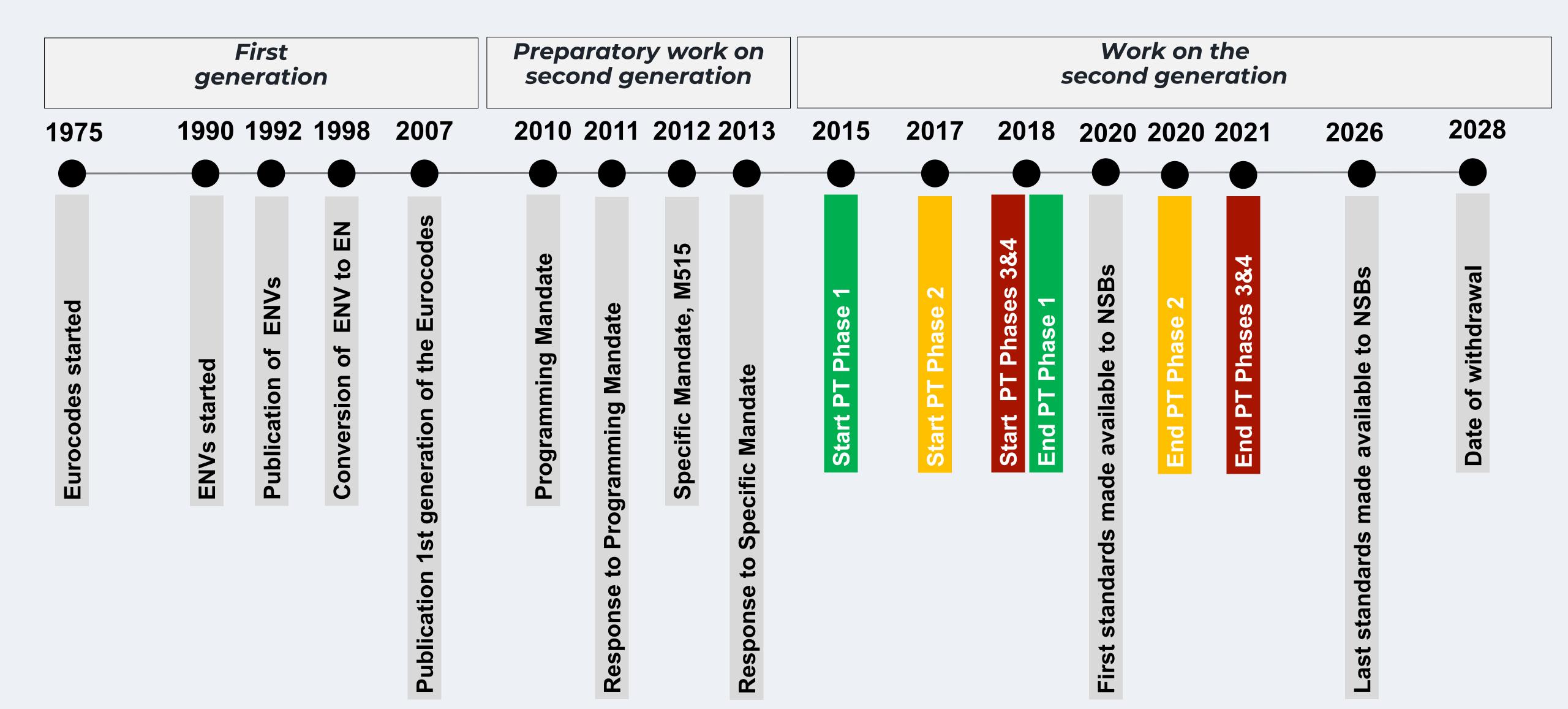
Achieving exemplary levels of international consensus

Over 480 formal decisions taken by CEN/TC 250 in last 11 years

Over 98% were taken unanimously

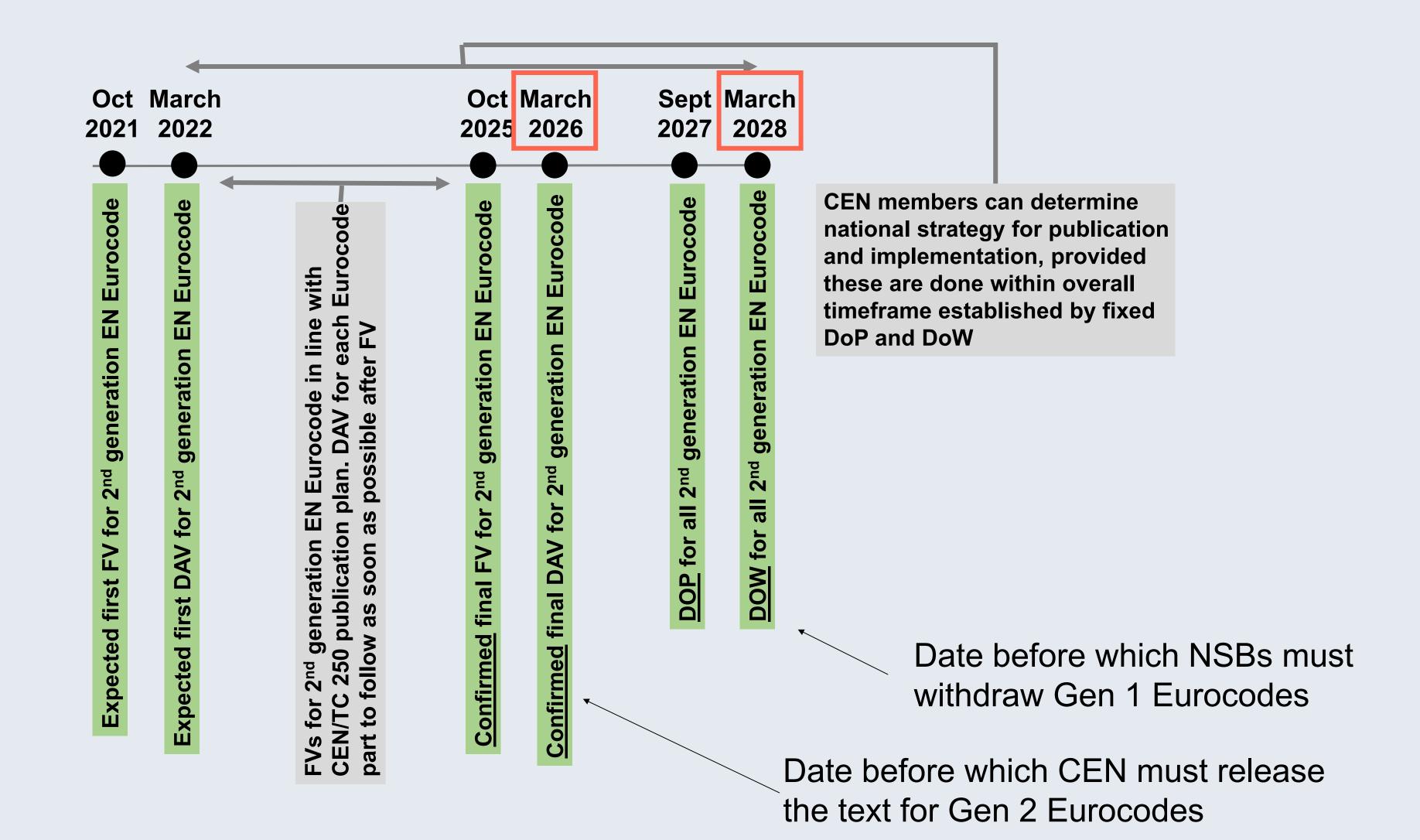


Second Generation Eurocode timeline



National Implementation





UK implementation strategy

National foreword

This British Standard is the UK implementation of EN 1993-1-1:2022. It supersedes BS EN 1993-1-1:2005+A1:2014, which will be withdrawn on 30 March 2028.

The UK participation in its preparation was entrusted to Technical Committee CB/203, Design & execution of steel structures.

A list of organizations represented on this committee can be obtained on request to its committee manager.

National choice is allowed in this standard where explicitly stated within notes. The National Annex to this standard contains the national choices to be used for buildings and civil engineering works constructed in the UK.

The first generation of EN Eurocodes was published between 2002 and 2007, with conflicting British Standards withdrawn in 2010. This document forms part of the second generation of EN Eurocodes.

The second generation of EN Eurocodes is expected to be published between 2023 and 2026. These documents are being published as soon as they are available. This is being done to enable users to prepare for the transition from the first generation to second generation of EN Eurocodes.

UK adoptions of the first generation of EN Eurocodes will be withdrawn by BSI on 30 March 2028. Until that date, the first generation documents should be considered as the applicable standards for buildings and civil engineering works constructed in the UK unless otherwise specified by the relevant authority or in the specification for a particular project.

This standard is intended to be used with its National Annex and other referenced documents, including other second generation Eurocodes, as an interdependent suite of documents.

While the use of provisions in this standard in conjunction with first generation Eurocodes is not precluded, it should be undertaken with care and should only be done when users are satisfied that it will not result in a lower level of reliability than the minimum level set in the first generation Eurocodes and associated UK National Annexes.

Positive confirmation that this document is 2nd generation

Explanation of reason for coexistence period

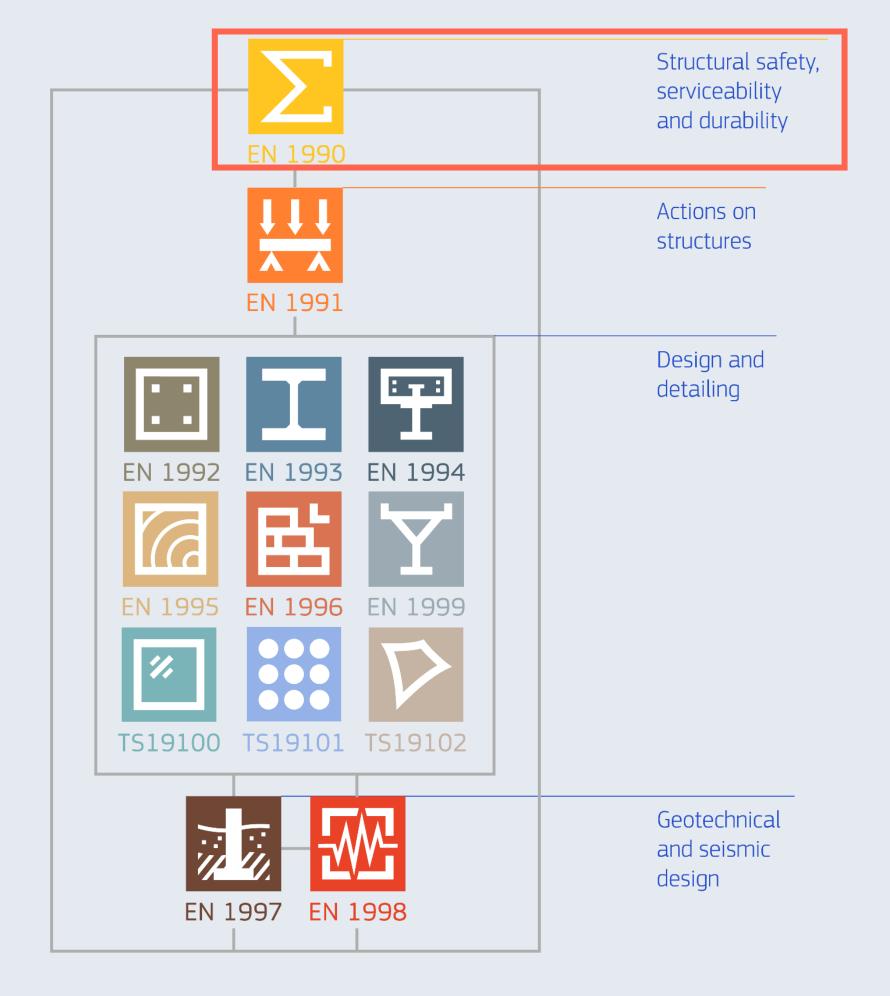
Statement of UK implementation strategy and DoW

Reference to Eurocodes as interdependent system of standards

Conditions for interim use of 2nd generation and 1st generation together



Eurocode Second Generation Updates EN 1990 Basis of Design and EN 1991 Actions on Structures





EN 1990

BRITISH STANDARD

BS EN 1990:2002

Eurocode — Basis of structural design

+A1:2005

corrigenda December 2008 and April 2010



ICS 91.010.30

English Version

FprA1

October 2025

Eurocode - Basis of structural and geotechnical design -Part 1: New structures

Eurocode - Bases des calculs structuraux et

EUROPEAN STANDARD

NORME EUROPÉENNE

EUROPÄISCHE NORM

Eurocode - Grundlagen der Planung von Tragwerken und geotechnischen Bauwerken - Teil 1: Neubauten

FINAL DRAFT

EN 1990:2023

Management Centre has the same status as the official versions.

This draft amendment is submitted to CEN members for formal vote. It has been drawn up by the Technical Committee CEN/TC

This draft amendment A1, if approved, will modify the European Standard EN 1990:2023. If this draft becomes an amendment, CEN members are bound to comply with the CEN/CENELEC Internal Regulations which stipulate the conditions for inclusion of this amendment into the relevant national standard without any alteration. This draft amendment was established by CEN in three official versions (English, French, German). A version in any other language made by translation under the responsibility of a CEN member into its own language and notified to the CEN-CENELEC

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Recipients of this draft are invited to submit, with their comments, notification of any relevant patent rights of which they are aware and to provide supporting documentation.

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COMITÉ EUROPÉEN DE NORMALISATION EUROPÄISCHES KOMITEE FÜR NORMUNG

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Ref. No. EN 1990:2023/FprA1:2025 E

EUROPEAN STANDARD NORME EUROPÉENNE

FINAL DRAFT FprEN 1990-2

EUROPÄISCHE NORM

ICS 91.010.30

Will supersede CEN/TS 17440:2020

English Version

Eurocode - Basis of structural and geotechnical design -Part 2: Assessment of existing structures

Eurocodes - Bases de calcul structuraux et géotechniques - Partie 2: Évaluation des structures

Eurocode - Grundlagen der Planung von Tragwerken und geotechnischen Bauwerken - Teil 2: Bewertung

This draft European Standard is submitted to CEN members for formal vote. It has been drawn up by the Technical Committee

If this draft becomes a European Standard, CEN members are bound to comply with the CEN/CENELEC Internal Regulations which stipulate the conditions for giving this European Standard the status of a national standard without any alteration.

This draft European Standard was established by CEN in three official versions (English, French, German). A version in any other language made by translation under the responsibility of a CEN member into its own language and notified to the CEN-CENELEC Management Centre has the same status as the official versions.

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COMITÉ EUROPÉEN DE NORMALISATION EUROPÄISCHES KOMITEE FÜR NORMUNG

CEN-CENELEC Management Centre: Rue de la Science 23, B-1040 Brussels

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ICS 91.010.30; 91.080.01



First generation

Second generation



EN 1990-1 Basic requirements

4.1 Basic requirements

- (1) The assumptions given in 1.2 and in the other Eurocodes shall be met.
- (2) A structure shall be designed and executed in such a way that it will, during its design service life, with appropriate degrees of reliability and in an economical way:
- sustain all reasonably foreseeable actions and influences that can occur during its execution and use, as specified for the structure;
- meet the specified serviceability requirements for the structure or a structural member;
- meet the specified durability requirements for the structure or a structural member.
- NOTE Design carried out in accordance with the Eurocodes is assumed to satisfy these requirements.
- (3) In the case of fire, the structural resistance shall be adequate for the required period of time.
- NOTE For general provisions related to fire design, see also EN 1991-1-2.

4.4 Robustness

- (1) A structure should be designed to have an adequate level of robustness so that during its design service life it will not be damaged by unforeseen adverse events to an extent disproportionate to the original cause.
- NOTE 1 Progressive collapse is an example of a damage that is disproportionate to the original cause.



EN 1990-1

Combinations of actions

8 Verification by the partial factor method

8.3.4.2 Combination of actions for persistent and transient (fundamental) design situations

- (2) When applying factors to actions, combinations of actions ΣF_{d} for persistent and transient (fundamental) design situations should be calculated by one of the following:
- Formula (8.12); or
- the most adverse of the two expressions in Formula (8.13); or
- the most adverse of the two expressions in Formula (8.14).

$$\sum F_{d} = \sum_{i} \gamma_{G,i} G_{k,i} + \gamma_{Q,1} Q_{k,1} + \sum_{j>1} \gamma_{Q,j} \psi_{0,j} Q_{k,j} + (\gamma_{P} P_{k})$$
(8.12)

or

$$\Sigma F_{d} = \begin{cases} \sum_{i} \gamma_{G,i} G_{k,i} + \gamma_{Q,1} \psi_{0,1} Q_{k,1} + \sum_{j>1} \gamma_{Q,j} \psi_{0,j} Q_{k,j} + (\gamma_{P} P_{k}) \\ \sum_{i} \xi_{i} \gamma_{G,i} G_{k,i} + \gamma_{Q,1} Q_{k,1} + \sum_{j>1} \gamma_{Q,j} \psi_{0,j} Q_{k,j} + (\gamma_{P} P_{k}) \end{cases}$$
(8.13)

or

$$\sum F_{d} = \begin{cases} \sum_{i} \gamma_{G,i} G_{k,i} + (\gamma_{P} P_{k}) \\ \sum_{i} \xi_{i} \gamma_{G,i} G_{k,i} + \gamma_{Q,1} Q_{k,1} + \sum_{j>1} \gamma_{Q,j} \psi_{0,j} Q_{k,j} + (\gamma_{P} P_{k}) \end{cases}$$
(8.14)



EN 1990-1 Basis of geotechnical design



6.3.2 Design values of the effects of actions

(2) In most cases, the following simplification can be made:

$$E_d = E\left\{\gamma_{F,i} F_{rep,i} ; a_d\right\} \quad i \ge 1 \tag{6.2a}$$

8.3.2 Design values of the effects of actions

$$E_{d} = E\left\{\Sigma F_{d}; a_{d}; X_{Rd}\right\} = E\left\{\Sigma \left(\gamma_{F} \psi F_{k}\right); a_{d}; X_{Rd}\right\} \quad (8.4)$$

First generation

Second generation

EN 1990-1 Combinations of actions

Table A.1.6 — Combinations of actions for serviceability limit states

Combinations	Characteristic	Frequent	Quasi- permanent	Seismic ^b		
General formula for effects of actions		(8.28)				
Formula for combination of actions	(8.29)	(8.30)	(8.31)	(8.32)		
Permanent $(G_{d,i})$	$G_{\mathrm{k},i}$	$G_{\mathbf{k},i}$	$G_{\mathbf{k},i}$	$G_{\mathbf{k},i}$		
Leading variable $(Q_{d,1})$	$Q_{\mathrm{k,1}}$	$\psi_{1,1}Q_{\mathrm{k},1}$	1h O	1h O		
Accompanying variable $(Q_{d,j})$	$\psi_{0,j}Q_{{f k},j}$	$\psi_{2,j}Q_{\mathbf{k},j}$	$\psi_{2,j}Q_{\mathbf{k},j}$	$\psi_{2,j}Q_{\mathbf{k},j}$		
Prestressing (P _d) ^a	$P_{\mathbf{k}}$	$P_{ m k}$	$P_{\mathbf{k}}$	$P_{\mathbf{k}}$		
Seismic (A _{Ed})	_	_	-	$A_{\mathrm{Ed,SLS}}$		

The characteristic value of prestressing $P_{\rm k}$ can be an upper, lower, or mean value. Guidance is given in the other Eurocodes.



Depending on the magnitude of A_{Ed,SLS}, the seismic combination of actions covers both the damage limitation (DL) and fully operational (OP) serviceability limit states defined in EN 1998 (all parts).

EN 1990-1 ULS partial factors

ULS partial factors
"Set B" "Set A" "Set C"

Table A.1.8 (NDP) — Partial factors on actions and effects for verification cases VC1 to VC4 for persistent and transient (fundamental) design situations

Action or effect			Partial factors $\gamma_{ m F}$ and $\gamma_{ m E}$ for verification cases					
Туре	Type Group Symbol Resulting effect			Structural resistance ^a	Static equilibrium and uplift ^b		Geotechnical design	
	Verific	ation case		VC1 ^a	VC2(a) ^b	VC2(b) ^b	VC3c	VC4 ^d
Permanent	Allf	$\gamma_{ m G}$	unfavourable	1,35k _F	1,35k _F	1,0	1,0	
action (G _k)	Waterl	γ_{Gw}	/destabilizin g	1,2 <i>k</i> _F	1,2 <i>k</i> _F	1,0	1,0	<i>c</i>
	Allf	$\gamma_{ m G,stb}$	stabilizingg	not used	1,15 ^e	1,0	not used	G _k is not factored
	Waterl	γ _{Gw,stb}			1,0e	1,0		
	All	$\gamma_{\rm G,fav}$	favourableh	1,0	1,0	1,0	1,0	
Prestressin g (P _k)		$\gamma_{ extsf{P}}^{ ext{k}}$						
Variable	Allf	$\gamma_{ m Q}$	nfarranabla	1,5 <i>k</i> _F	1,5 <i>k</i> _F	1,5 <i>k</i> _F	1,3	$\gamma_{ m Q,red}^{ m j}$
action (Q _k)	Waterl	$\gamma_{ m Qw}$	unfavourable	1,35k _F	1,35k _F	1,35k _F	1,15	1,0
	All	$\gamma_{ m Q,fav}$	favourable			0		
Effects of act	Effects of actions (E)		unfavourable				1,35 <i>k</i> _F	
		$\gamma_{\rm E,fav}$	favourable	γ _E is not applied			1,0	



First generation sets



$$a = 5m$$

$$\beta = \frac{b}{a}$$

$$\beta^2 = 0,5$$

$$R_A = \frac{a}{2} \left[\gamma_{G,stb} - \gamma_G \beta^2 - \gamma_Q x \beta^2 \right]$$

$$R_A < 0$$

$$R_A = g_{1,k} = g_{2,k} = g_k$$

$$x = \frac{q_k}{g_k}$$

$$R_A > 0$$

$$R_A < 0$$

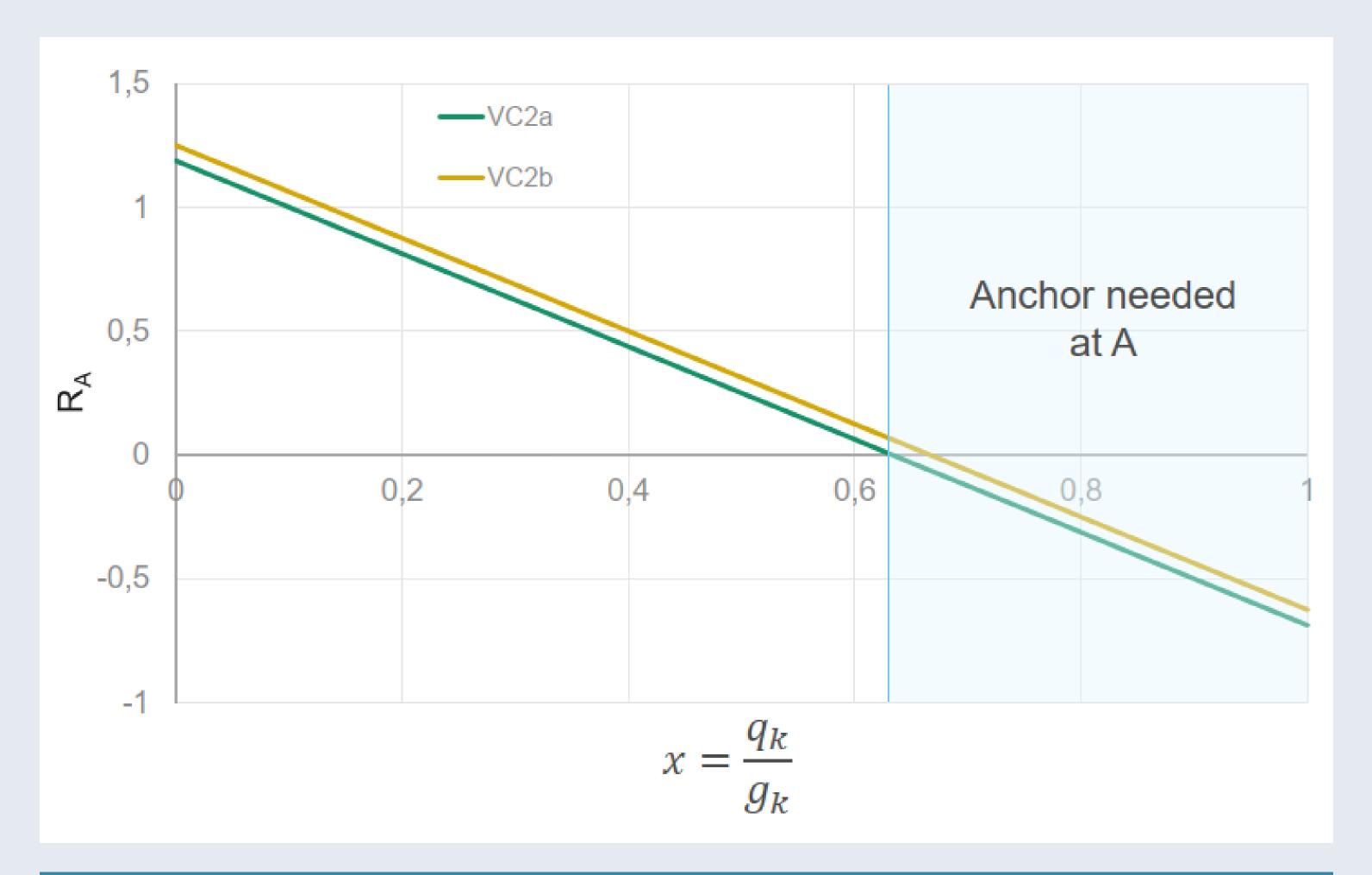
EN 1990-1 **EQU equilibrium changes**"Set B" "Set A" "Set C" Table A.1.8 (NDP) — Partial factors on actions and effects for verification cases VC1 to VC4 for

persistent and transient (fundamental) design situations

Action or effect			Partial factors $\gamma_{\rm F}$ and $\gamma_{\rm E}$ for verification cases					
Туре	Group	Symbol	Resulting effect	Structural resistance ^a	•		Geotechnical design	
	Verific	ation case		VC1 ^a	VC2(a) ^b	VC2(b)b	VC3c	VC4 ^d
Permanent	Allf	$\gamma_{ m G}$	unfavourable	1,35k _F	1,35k _F	1,0	1,0	
action (G _k)	Water ^l	$\gamma_{ m Gw}$	/destabilizin g	1,2 <i>k</i> _F	1,2 <i>k</i> _F	1,0	1,0	
	Allf	$\gamma_{\rm G,stb}$	stabilizingg	not used	1,15 ^e	1,0	not used	<i>G</i> _k is not factored
	Waterl	$\gamma_{ m Gw,stb}$			1,0e	1,0		
	All	$\gamma_{\rm G,fav}$	favourableh	1,0	1,0	1,0	1,0	
Prestressin g (P _k)		$\gamma_{ extsf{P}}^{ ext{k}}$						
Variable	Allf	$\gamma_{ m Q}$	unfavourable	1,5 <i>k</i> _F	1,5 <i>k</i> _F	1,5 <i>k</i> _F	1,3	$\gamma_{ m Q,red}^{ m j}$
action (Q _k)	Waterl	$\gamma_{ m Qw}$	umavourable	1,35k _F	1,35k _F	1,35k _F	1,15	1,0
	All	$\gamma_{ m Q,fav}$	favourable			0		
Effects of act	Effects of actions (E)		unfavourable	-	ia not applied			1,35 <i>k</i> _F
		$\gamma_{\rm E,fav}$	favourable		_E is not applied			1,0



First generation sets





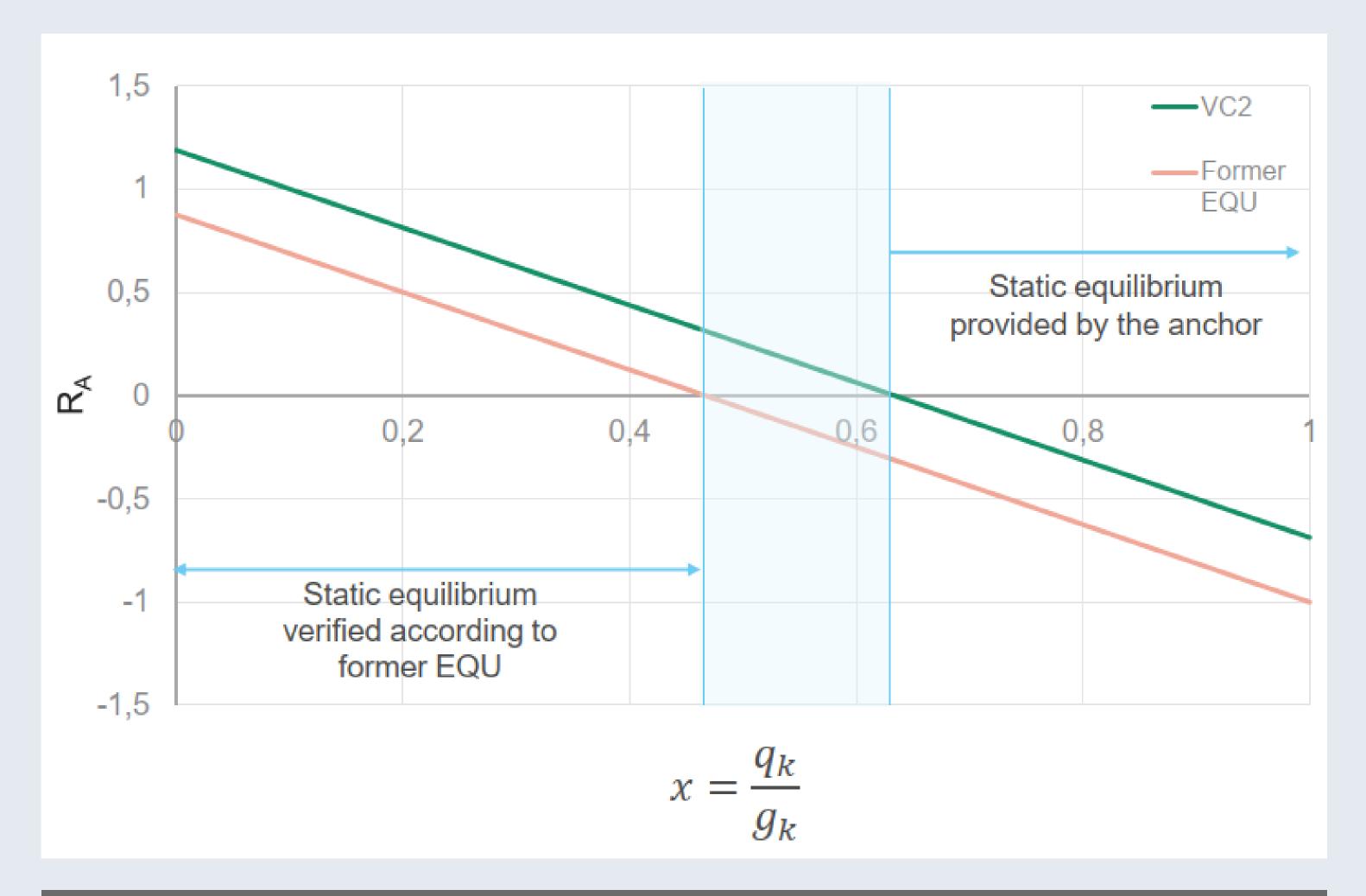




Table A.1.8 (NDP) — Partial factors on actions and effects for verification cases VC1 to VC4 for persistent and transient (fundamental) design situations

Action or effect			Partial factors $\gamma_{\rm F}$ and $\gamma_{\rm E}$ for verification cases					on cases		
Type	Group	Symbol	Resulting effect	Structural resistance ^a		Static equilibrium and uplift ^b		Geotechnical design		
	Verific	ation case	•	VC1 ^a		VC2(a) ^b	VC2(b)b	J	/C3 c	VC4 ^d
Permanent	Allf	$\gamma_{ m G}$	unfavourable	1,35k _F	,	1,35 <i>k</i> _F	1,0	Г	1,0	
action (G _k)	Waterl	γ_{Gw}	/destabilizin g	1,2 <i>k</i> _F		1,2 <i>k</i> _F	1,0		1,0	C : t
	Allf	$\gamma_{ m G,stb}$	atabiliain as	t		1,15 ^e	1,0	K		G _k is not factored
	Waterl	γ _{Gw,stb}	stabilizing ^g	not used		1,0 ^e	1,0	used		
	All	$\gamma_{\rm G,fav}$	favourableh	1,0		1,0	1,0		L,0	
Prestressin g (P _k)		γ_{P}^{k}								
Variable	Allf	$\gamma_{ m Q}$		1,5 <i>k</i> _F		$1,5k_{ m F}$	1,5 <i>k</i> _F	7	1,3	$\gamma_{ m Q,red}^{ m j}$
action (Q _k)	Waterl	$\gamma_{ m Qw}$	unfavourable	1,35k _F		$1,35k_{ m F}$	1,35k _F	1	1,15	1,0
	All $\gamma_{Q,fa}$		favourable				0			
Effects of act	Effects of actions (E)		unfavourable				1,35 <i>k</i> _F			
		$\gamma_{\rm E,fav}$	favourable	γ _E is not applied				1,0		



EN 1990-1 Robustness

4.4 Robustness

- (1) A structure should be designed to have an adequate level of robustness so that during its design service life it will not be damaged by unforeseen adverse events to an extent disproportionate to the original cause.
- NOTE 1 Progressive collapse is an example of a damage that is disproportionate to the original cause.
- NOTE 2 For most structures, design in accordance with the Eurocodes is assumed to provide an adequate level of robustness without the need for any additional design measures to enhance structural robustness.
- (2) Design measures to enhance structural robustness should be applied when specified by the relevant authority or, where not specified, as agreed for a specific project by the relevant parties.
- NOTE 1 Guidance on additional design measures to enhance structural robustness for buildings and bridges is given in Annex E.
- NOTE 2 Further guidance can be given in the National Annex.



EN 1990-1 Robustness

Annex E

(informative)

Additional guidance for enhancing the robustness of buildings and bridges

Table E.1 —Design for identified accidental actions and design strategies for enhanced robustness

(EN Explicit	Design for accidental actions (EN 1991 (all parts)) Explicit design of the structure (e.g. against explosion, impact)		Design for enhanced robustness (EN 1990) Strategies based on limiting the extent of damage				
Design struto resist action	<u>the</u>	Prevent or reduce the action e.g. protective measures, control of events	Alternative load paths either providing sufficient ductility, resistance and deformation capacity and redundancy, or applying prescriptive design rules	i.e. designing selected members to resist notional action(s)	i.e. separation into distinct parts		



Indicative national choice – draft NA

EN 1990-1 Robustness

Table E.2 — Indicative

rable E.Z — illulcativ				
Consequence class				
CC3	V			
	S			
	p			
	a			
	a			
	b			
	c] d			
	d			
CC2	V			
	S			
	p			
	a			
	b			
	c			
CC1	N			
	n			

Table NA.E.2 – Design methods for enhancing robustness for buildings					
Consequence class Design methods					
CC3	A systematic risk assessment of the building should be undertaken taking into account all the normal hazards that can reasonably be foreseen, together with any abnormal hazards. Critical situations for design should be selected that reflect the conditions that can reasonably be foreseen as possible during the life of the building.				
	The structural form and concept and any protective measures should then be chosen and the detailed design of the structure and its elements undertaken in accordance with the Eurocodes.				
CC2b	In addition to the measures listed for CC1, either:				
Upper risk group	 a) for framed and load-bearing wall construction, provide effective horizontal ties, together with effective vertical ties in all supporting columns and walls; or b) check that upon the notional removal of each supporting column and each beam supporting one or more columns, or any nominal length of load-bearing wall (one at a time in each storey of the building), the building remains stable and that the area of floor at any storey does not exceed the tolerable limit. Where the notional removal of such columns and lengths of walls would result in an extent of damage in excess of the tolerable limit, then such elements should be designed as a key element. 				
CC2a Lower risk group	In addition to the measures listed for CC1, for framed and load-bearing wall construction, provide effective horizontal ties, or effective anchorage of suspended floors to walls.				
CC1	Provided the structure is designed in accordance with other provisions in the Eurocodes, no additional measures are likely to be necessary.				



Indicative national choice – draft NA

EN 1990-1 Robustne

Table A.1.1 (NDP) -

Consequence class	
CC4a	
CC3	
CC2	
CC1	
CC0a	
a For provisions c	once

Table NA.1 – Table A.1.1 (NA) – Examples of buildings in different consequence classes

	Consequence class	Description of consequence	Example of categorization of building type and occupancy a
	CC4	Highest	Critical infrastructure, (e.g. parts of a nuclear or chemical plant), when specified by the relevant authority or, where not specified, agreed for a specific project by the relevant parties
	CC3b	High (upper class)	Buildings defined for CC3a, where an increased level of reliability is required, when specified by the relevant authority or, where not specified, agreed for a specific project by the relevant parties
	CC3a	High (lower class)	All buildings that exceed the limits on area and number of storeys defined for CC2b
ł			All buildings to which members of the public are admitted in significant numbers
-			Stadia accommodating more than 5 000 spectators
			Buildings containing hazardous substances and/or processes
	CC2b	Normal (upper class)	Hotels, flats, apartments and other residential buildings greater than 4 storeys but not exceeding 15 storeys
		(-	Educational buildings greater than single storey but not exceeding 15 storeys
			Retailing premises greater than 3 storeys but not exceeding 15 storeys
			Hospitals not exceeding 3 storeys
			Offices greater than 4 storeys but not exceeding 15 storeys
			All buildings to which the public are admitted and which contain floor areas exceeding 2 000 m ² but not exceeding 5 000 m ² at each storey
•			Car parking not exceeding 6 storeys
	CC2a	Normal	5 storey single occupancy houses
		(lower class)	Hotels not exceeding 4 storeys



EN 1990-1 Reliability differentiation

Table A.1.8 (NDP) — Partial factors on actions and effects for verification cases VC1 to VC4 for persistent and transient (fundamental) design situations

Action or effect			Partial factors γ_{F} and γ_{E} for verification cases					
Туре	Group	Symbol	Resulting effect	Structural resistance ^a	Static equilibrium and uplift ^b		Geotechnical design	
	Verific	ation case	•	VC1 ^a	VC2(a)b	VC2(b) ^b	VC3c	VC4 ^d
Permanent	Allf	$\gamma_{ m G}$	unfavourable	$1,35 k_{ m F}$	1,35k _F	1,0	1,0	
action (G _k)	Waterl	$\gamma_{ m Gw}$	/destabilizin g	1,2 <i>k</i> _F	1,2 <i>k</i> _F	1,0	1,0	
	Allf	$\gamma_{ m G,stb}$	stabilizingg	not used	1,15 ^e	1,0	not used	G _k is not factored
	Waterl	γ _{Gw,stb}			1,0e	1,0		
	All	$\gamma_{\rm G,fav}$	favourable ^h	1,0	1,0	1,0	1,0	
Prestressin g (P _k)		γ_{P}^{k}						
Variable	Allf	$\gamma_{ m Q}$	unfarraunabla	1,5 <i>k</i> _F	1,5 <i>k</i> _F	1,5 <i>k</i> _F	1,3	$\gamma_{ m Q,red}^{ m j}$
action (Q _k)	Waterl	$\gamma_{ m Qw}$	unfavourable	1,35k _F	1,35k _F	1,35k _F	1,15	1,0
	All	$\gamma_{ m Q,fav}$	favourable	0				
Effects of act	Effects of actions (E) $\gamma_{\rm E}$		unfavourable	w is not smalled			1,35k _F	
		$\gamma_{\rm E,fav}$	favourable	γ _E is not applied 1,0			1,0	



EN 1990-1 Reliability differentiation

Table NA.4 – Table A.1.9 (NA) – Consequence factors for buildings and geotechnical structures

Consequence class (CC) ^a	Description of consequences	Consequence factor k _F
CC3b	High (upper class)	1,1
CC3a	High (lower class)	
CC2	Normal (upper class)	1,0
CC1b	Low (upper class)	
CC1a	Low (lower class)	0,9

^a The provisions in Eurocodes cover design rules for structures classified as CC1 to CC3, see 4.3. For CC4 structures, additional provisions to those given in the Eurocodes are needed, e.g. reliability-based or risk-informed approaches.

^b Values of $k_F = 1,1$ for CC3b or $k_F = 0,9$ for CC1a structures are used when specified by the relevant authority or, where not specified, agreed for a specific project by the parties with appropriate justification.

Indicative national choice – draft NA

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CONSTRUCTION						

CC1b	Low	Single occupancy houses not exceeding 4 storeys
	(upper class)	Buildings defined for CC1a, where an increased level of reliability is required when specified by the relevant authority or, where not specified, agreed for a specific project by the relevant parties.
CC1a	Low	Where a reduced level of reliability is acceptable, when specified by
	(lower class)	the relevant authority or, where not specified, agreed for a specific project by the relevant parties
		Agricultural buildings with low human occupancy (Class 2 in accordance with BS 5502-22:2003+A1:2013)
		Buildings into which people rarely go, provided no part of the building is closer to another building, or area where people do go, than a distance of 1,5 times the building height
CC0	Lowest	Elements other than structural

EN 1990

BRITISH STANDARD

ICS 91.010.30; 91.080.01

BS EN 1990:2002 +A1:2005

corrigenda December 2008 and April 2010

Eurocode — Basis of structural design

EUROPEAN STANDARD NORME EUROPÉENNE EUROPÄISCHE NORM

FINAL DRAFT EN 1990:2023

FprA1

October 2025

ICS 91.010.30

English Version

Eurocode - Basis of structural and geotechnical design -Part 1: New structures

Eurocode - Bases des calculs structuraux et

Eurocode - Grundlagen der Planung von Tragwerken und geotechnischen Bauwerken - Teil 1: Neubauten

This draft amendment is submitted to CEN members for formal vote. It has been drawn up by the Technical Committee CEN/TC

This draft amendment A1, if approved, will modify the European Standard EN 1990:2023. If this draft becomes an amendment, CEN members are bound to comply with the CEN/CENELEC Internal Regulations which stipulate the conditions for inclusion of this amendment into the relevant national standard without any alteration.

This draft amendment was established by CEN in three official versions (English, French, German). A version in any other language made by translation under the responsibility of a CEN member into its own language and notified to the CEN-CENELEC Management Centre has the same status as the official versions.

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Ref. No. EN 1990:2023/FprA1:2025 E

EUROPEAN STANDARD NORME EUROPÉENNE

FINAL DRAFT FprEN 1990-2

EUROPÄISCHE NORM

ICS 91.010.30

English Version

Eurocode - Basis of structural and geotechnical design -Part 2: Assessment of existing structures

Eurocodes - Bases de calcul structuraux et géotechniques - Partie 2: Évaluation des structures

Eurocode - Grundlagen der Planung von Tragwerken und geotechnischen Bauwerken - Teil 2: Bewertung

Will supersede CEN/TS 17440:2020

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First generation

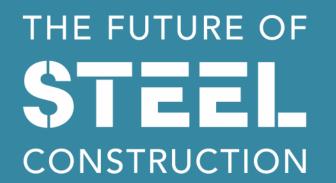
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Second generation

UK approach to assessment







EN 1990-1

4.1 Basic requirements

- (1) The assumptions given in 1.2 and in the other Eurocodes shall be met.
- (2) A structure shall be designed and executed in such a way that it will, during its design service life, with appropriate degrees of reliability and in an economical way:
- sustain all reasonably foreseeable actions and influences that can occur during its execution and use, as specified for the structure;

meet the specified serviceability requirements for the structure or a structural member;

EN 1990-2

meet the spe

NOTE Design

NOTE

4.1 Basic requirements

- (1) The assumptions given in 1.2 and in the other Eurocodes shall be met.
- (2) The assessment of an existing structure shall verify that the structure fulfils the specified (3) In the case of requirements during the remaining service life.
 - For ger NOTE 1 Additional conditions for existing structures to which this document applies can be given in the National Annex.
 - NOTE 2 The basic requirements for an existing structure can be different from the basic requirements applicable for a new structure.

Minimum requirements for the verification where the structure includes new and existing parts can be NOTE 3 given in the National Annex.



5 Principles of assessment

5.1 General

5.1.1 Assessment process

(1) The assessment of a structure may be carried out following a <u>stepwise process</u> with increasing levels of detail and accuracy.

NOTE 1 A stepwise process can include preliminary and detailed stages in order to optimize the overall level of effort required for the assessment.



- (3) Available information ahead of the assessment of an existing structure should be checked and taken into consideration where relevant, including from:
- the original design and construction record;
- previous condition surveys;
- inspections carried out during the past service life, monitoring;
- previous assessment reports;
- previous rehabilitation and/or structural modifications;
- information about significant environmental, seismic or other extreme events occurred after construction;
- information about changes in ground conditions occurred after construction.



5.1.2 Assessment scope and objectives

- (2) The assessment scope and objectives should include the following:
- the extent of the structure to be assessed;
- the requirements to be fulfilled in the remaining service life;
- the assessment situations to be considered for the structure, including those related to possible changes in structural conditions or actions;
- the actions to be considered according to the relevant assessment situations;
- the limit states to be assessed and the methods of assessment for the relevant limit states;
 - NOTE For verification of the serviceability limit state, see 5.4.
- the format for describing the outcome of the assessment.
 - EXAMPLE For example in terms of a calculated operational restriction for a particular action.



5.1.3 Assessment approach

- (1) The assessment approach and the assumptions for the assessment shall be specified and documented, including:
- a) the method of assessment;
- the approach for assessing the effects of structural condition, deterioration, construction process and subsequent changes to the structure, if relevant;
- c) the data for the basic variables used in the assessment;
- d) the structural analysis methodology;
- e) the verification methods.



8.3 Verification of ultimate limit states (ULS)

8.3.1 General

- (1) When verifying ultimate limit states EN 1990:2023, 8.3 should be applied, unless otherwise specified, substituting where appropriate the values of design parameters with the corresponding values for assessment.
- NOTE 1 Combinations of actions for assessment are given in EN 1990:2023, 8.3, unless the National Annex defines other combinations of actions.
- NOTE 2 Partial factors can be (i) fixed (standardized for use in a country), valid for a range of cases, or (ii) adjusted for a specific case.
- NOTE 3 Fixed partial factors for actions are used, unless conditions for the use of adjusted partial factors for actions are given in the National Annex.
- NOTE 4 For fixed partial factors for actions and combination factors ψ , see Annex A.



NA to PD CEN/TS 17440:2020 – indicative of national choice

The values of all partial factors for actions and ψ factors for assessment shall be as specified by the relevant authority.

Where no values of partial factors for actions and ψ factors for assessment are specified by the relevant authority, values may be agreed with the relevant parties.

Partial factors that implicitly include ψ factors may be used as an alternative to setting ψ factors for assessment.

Partial factors for actions may be split into factors relating to uncertainty in the magnitude of the action and uncertainty in the model effects.

In the absence of agreed values of partial factors for actions and ψ factors between the relevant parties, the values should be taken as the corresponding values for design given in BS EN 1990 (together with its UK National Annex) and BS EN 1991 (all parts, together with their UK National Annexes).

NOTE 1: It is common practice in UK bridge assessments to use partial factors for actions Y_{fL} that are defined for each combination of actions (implicitly including ψ factors), and to apply an additional partial factor Y_{f3} accounting for uncertainty in the model effects.

NOTE 2: It is common practice in the UK to apply fixed default values for partial factors for actions, rather than calculate partial factors on a project basis.

A.1 General application and appl

A.1.7 Partial factors for ultimate lin

(1) Partial factors for ultimate limit states

NOTE EN 1990:2023, A.1.7 applies, unles



8.3.2 Assessment of resistance

- (2) The assessment values of resistance shall be determined from resistance models that are consistent with the information of the existing structure related to:
- material properties;
- structural detailing;
- geometry;
- structural conditions.

NOTE 1 Structures that were designed and constructed to withdrawn standards can have material properties, detailing arrangements and execution tolerances that do not comply with or are not covered by current standards. Particular attention is needed in the implementation of resistance models from current standards valid for new structures, which implicitly or explicitly rely on design requirements for material properties, detailing arrangements and execution tolerances being satisfied. Further guidance can be found in the relevant Eurocodes.

NOTE 2 Structures that do not comply with current design standards are not necessarily unsafe. The use of updated values for basic variables and refined resistance models for the assessment that explicitly take into account deficiencies can be particularly beneficial in accurately assessing the resistance of existing structures.



- (4) In absence of specific assessment resist the Eurocodes, valid for design, should be u • in good condition and have
- material properties,
- detailing provisions, and
- execution tolerances

that satisfy

- the requirements of the relevant Eurocc
- the related product standards, and
- execution standards.

The National Annex can provide app NOTE

NA to PD CEN/TS 17440:2020 – indicative of national choice

The approach for assessing the structural resistance of

- structures that are not within the scope of the Eurocodes;
- structures that do not satisfy the requirements of the respective material-oriented Eurocodes (and the related product standards and execution standards) with respect to material properties, detailing arrangements and execution tolerances;
- structures exhibiting deterioration;

should be as specified by the relevant authority or, where not specified, agreed for a specific project by the relevant parties.

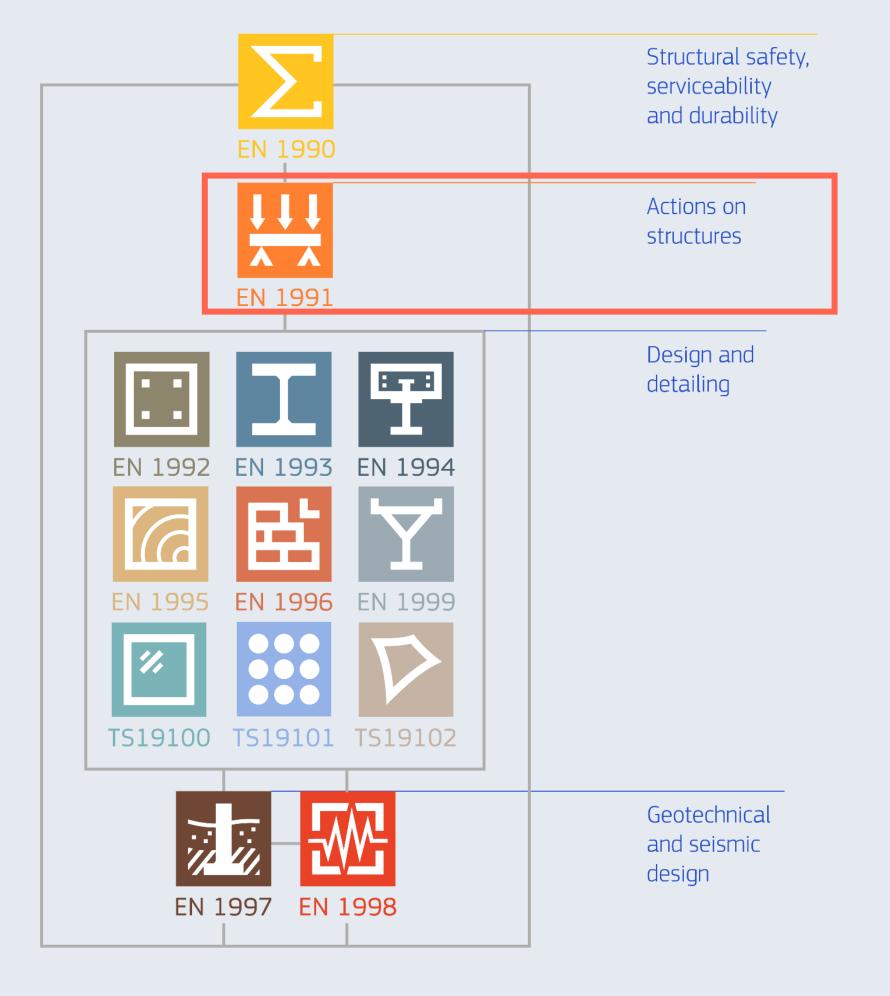
Guidance for assessment of resistance for buildings can be found NOTE: in BRE Digest 366.

Criteria for assessment of resistance for cast iron bridge NOTE: structures and masonry arch bridge structures are included in CS 454.

resistance models in the Eurocodes valid for des NOTE: Methods for assessing the structural resistance of common types of bridge structure found in the UK, including assessment of the effects of deterioration, can be found in the Design Manual for Roads and Bridges, including CS 454, CS 455, CS 456, and CS457.



Eurocode Second Generation Updates EN 1990 Basis of Design and EN 1991 Actions on Structures





EN 1991-1-1 Imposed loads

EN 1990-1

elements other than structural

completion and finishing elements connected with the structure that are not classified as structural members and that have the lowest consequence of failure

Note 1 to entry: See 4.3 for the classification of consequences of failure.

EXAMPLE Roofing; surfacing and coverings; partitions and linings; kerbs; wall cladding; suspended ceilings; thermal insulation; bridge furniture, road surfacing; services fixed permanently to, or within, the structure such as equipment for lifts and moving stairways; heating, ventilating and air conditioning equipment; electrical equipment; pipes; cable trunking and conduits.



EN 1991-1-1 Imposed loads

Table 6.1 —	(NDP)	Categories of	of use and	l values	for q_k and Q_k	
I abic oil	INDI	Categories	or use and	i vaiues	ivi ykanu yk	

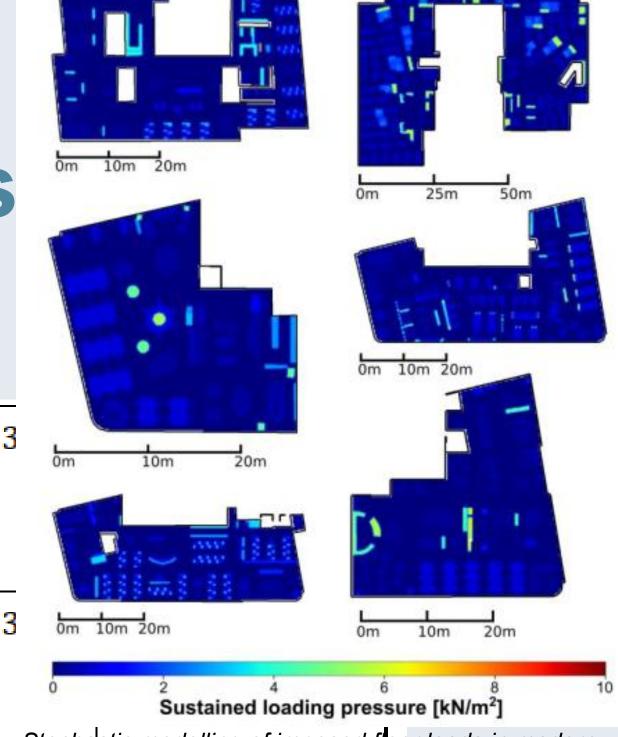
Category	Specific Use	Sub-categories with examples	q _k [kN/m ²]	Q _k [kN]	Typical dimension of the area loaded by Qk expressed in (m × m)
A	Areas for domestic and residential activities	A1 Rooms in residential buildings and houses, including corridors.	2,0	2,0	0,05 × 0,05
		A2 Bedrooms, wards, dormitories, private bathrooms and toilets in hospitals, hotels, hostels and other institutional residential occupancies.	2,0	2,0	0,05 × 0,05
Ba	Public areas (not susceptible to crowding)	B1 Office areas for general use including corridors other than archive / storage areas (see Category E)	3,0	3,0	0,05 × 0,05
		B2 Kitchens, communal bathrooms and toilets in hospitals, hotels, hostels and other institutional residential occupancies.	3,0	3,0	0,05 × 0,05
Cp'c'q	Public areas where people can congregate (with the exception of areas defined under category A, B, and D)	C1: Areas with tables, etc. e.g. areas in schools, cafés, restaurants, dining halls, reading rooms, receptions.	3,0	4,0	0,05 × 0,05
		C2: Areas with fixed seats, e.g. areas in churches, theatres, cinemas, conference rooms, lecture halls, assembly halls, waiting rooms.	4,0	4,0	0,05 × 0,05
		C3: Areas without obstacles for moving people, e.g. areas in museums, exhibition rooms, etc. and corridors to areas not belonging to categories A1, B1 and C5.	5,0	4,0	0,05 × 0,05
		C4: Areas with possible physical activities, e.g. dance halls, gymnastic rooms, stages.	5,0	7,0	0,05 × 0,05

Category	Specific Use	Sub-categories with examples	q _k [kN/m ²]	Q _k [kN]	Typical dimension of the area loaded by $Q_{\mathbf{k}}$ expressed in $(\mathbf{m} \times \mathbf{m})$
		C5: Areas susceptible to large crowds, e.g. in buildings for public events including corridors like concert halls, sports halls including stands, and railway platforms.	7,5	4,5	0,05 × 0,05
D	Shopping areas	D1: Areas in retail shops	4,0	4,0	0,05 × 0,05
	areas	D2: Areas in department stores	5,0	7,0	0,05 × 0,05
Е	Areas for archive, storage and	E1: Areas susceptible to accumulation of goods, including access areas ^f	7,5	7,0	a
	industrial use ^e	E2: Industrial use g.h.i.j	a		
F	Garages and vehicle traffic areas (excluding ordinary	Gross vehicle weight ≤ 30 kN: F1 Traffic and parking areas for light vehicles (≤8 seats not including driver) e.g. garages; parking areas, parking halls	2,5	20	a
G	roads and bridges)	30 kN < Gross vehicle weight ≤ 160 kN: G1 Traffic and parking areas for medium vehicles (on 2 axles) e.g. access routes, delivery zones, zones accessible to fire engines	5,0	90	0,2 × 0,2
		Gross vehicle weight > 160 kN: G2 Traffic and parking areas for heavy vehicles k	a		
H 1		s not accessible except for normal ntenance and repair		1,0	0,05 × 0,05
I	Roofs accessible with occupancy according to categories A to G		See categories A to G		
K	Roofs accessible for special services, such as classes HC for helicopter landing areas		5,0	5,0 See Table 6.4	
S	Stairs and landings	S1 Stairs and landings to areas belonging to category A1 and B1. ^m	See categ and	•	0,05 × 0,05
		S2 Stairs and landings for tribunes without fixed seats that are defined as escape ways. ^m	7,5	3,0	0,05 × 0,05
		S3 Stairs and landings not belonging to category S1 or S2. ^m	5,0	2,0	0,05 × 0,05

STEEL CONSTRUCTION

EN 1991-1-1 Imposed loads Office floor loading

Ba	Public areas (not susceptible to	B1 Office areas for general use including corridors other than archive / storage areas (see Category E)	3,0	
	crowding)	B2 Kitchens, communal bathrooms and toilets in hospitals, hotels, hostels and other institutional residential occupancies.	3,0	



Stochastic modelling of imposed floor loads in modern office buildings, Hawkins et al (under peer review)

Category	Specific Use	Sub-categories with examples	q _k [kN/m²]	Q _k [kN]
B Offices and communal	B1 Office areas for general use other than archive / storage areas (see Category E)			
	areas for non- domestic	B11 Office areas other than those covered in B12	2.5	2.7
residential activities	B12 Office areas at or below ground floor level; corridors, stairs and landings in offices	3.0	2.7	
		B2 Communal areas (kitchens and communal bathrooms and toilets) in residential occupancies for non-domestic use such as hospitals, hotels, hostels, student accommodations.	3.0	2.0

Indicative national choice – draft NA

STEEL CONSTRUCTION

EN 1991-1-1 Imposed loads Car park loading

F Garages and vehicle traffic areas (excluding ordinary

Gross vehicle weight ≤ 30 kN:

F1 Traffic and parking areas for light vehicles (≤8 seats not including driver) e.g. garages; parking areas, parking halls



Category	Specific Use	Sub-categories with examples	q _k [kN/m²]	Q _k [kN]
F	Garages and vehicle traffic areas (excluding ordinary roads and bridges) (see NOTE 1)	Gross vehicle weight ≤ 32 kN: F1 Traffic and parking areas for light vehicles (≤8 seats not including driver) e.g. garages; parking areas, parking halls	3.0	30 kN (axle load to be divided by two wheels as in Figure 6.5 to BS EN 1991-1-1:2025; loaded area per wheel is 0.2 × 0.2 (m × m) or 15 kN (jack load) applied to an area 0.05 × 0.05 (m × m)

Indicative national choice – draft NA

STEEL CONSTRUCTION



EN 1991-1-3 Snow

3.1.5

balanced snow load arrangement on the roof

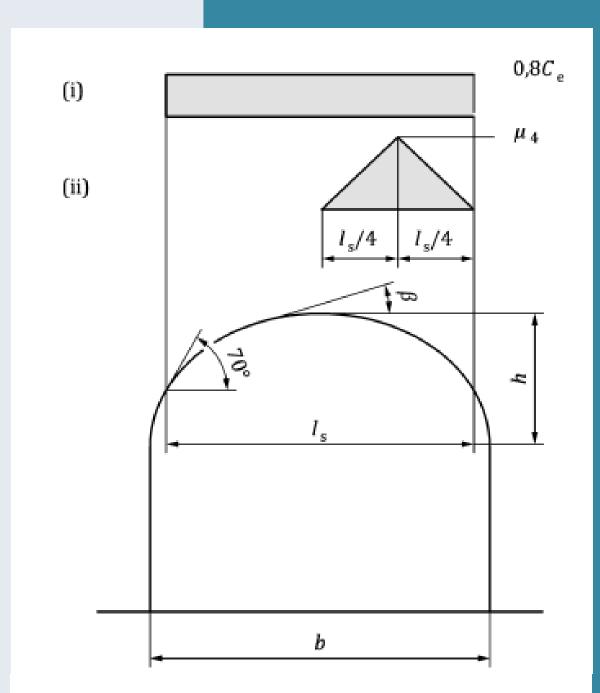
load arrangement which describes the uniformly distributed snow load on the roof, affected by the shape of the roof and its exposure to wind

3.1.6

unbalanced snow load arrangement on the roof

load arrangement which describes the snow load distribution resulting from snow having been moved from one location to another location on a roof or off the roof, depending on the exposure of the roof to wind and the effects of sliding

Note 1 to entry: Unbalanced load arrangements given in this document assume that wind can have any direction.



Key

- (i) balanced load arrangement
- (ii) unbalanced load arrangement

EN 1991-1-3 Snow

6.1 Characteristic values

(1) The characteristic value of snow load on the ground (s_k) should be determined in accordance with EN 1990:2023, 6.1.2.3(2) and the definition for characteristic snow load on the ground given in 3.1.1.

NOTE 1 Characteristic values of snow load on the ground at sites for altitudes up to 1 500 m can be set by the National Annex.

(3) The effects of climate change shall be taken into account.

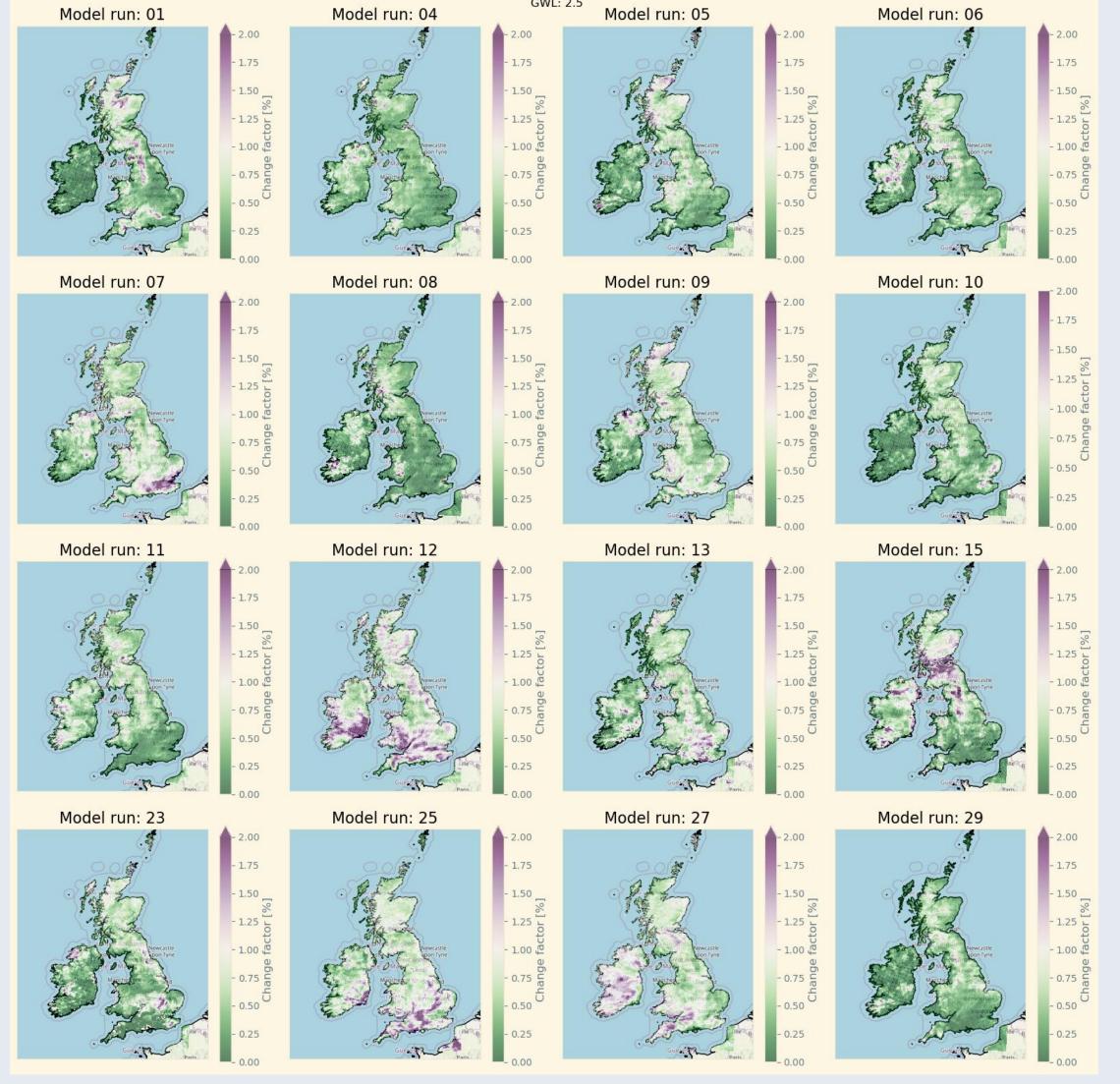
NOTE 1 The effects of climate change are taken into account by multiplying the characteristic value of snow load on the ground (s_k) by a scaling factor, $f_{s,cc}$, greater than or equal to 1, unless the National Annex gives a different approach.

NOTE 2 When the scaling factor approach is used, minimum values for the scaling factor $f_{s,cc}$ can be set in the National Annex.

(4) Additional project-specific requirements to account for the effects of climate change should be as specified by the relevant authority or, where not specified, may be agreed for a specific project by the relevant parties.



Climate change Factor of change approach





EN 1991-1-4 Wind

Wind conditions	Aerodynamics	Structural responses
1. Basic velocity pressure	a) Buildings and cladding	a) Along-wind response
Fundamental basic wind velocity v_{b0} [6.2(1), Note 1] Modification c_{alt} , c_{dir} , c_{season}	Reference height z _e [Annex B] External wind pressure	Simplifications: e.g. buildings with a height $h \le 15$ m or natural frequency $n_1 > 5$ Hz [8.2]
[6.2(4), Note 1-Note 3]	External pressure coefficient c_{pe} [B.3-B.5]	Not relevant: c_{sd} =1,0
Probability factor c_{prob} [Formula (6.2)]	External surface pressure p	Detailed procedure, or no simplification
Basic wind velocity v_b [Formula (6.1)]	[Formula (7.2)]	allowed ([8.2] otherwise)
Reference basic mean velocity pressure q _b [Formula (6.3)]	Influence of envelope permeability Internal pressure	b) Across-wind and torsional response
2. Terrain effects	coefficient c_{pi} [B.6]	Buildings: Dependent on slenderness
Terrain category (Table 6.1 (NDP), A.3, A.4)	Internal surface pressure p [Formula (7.3)]	ratio $h/\sqrt{(b \cdot d)}$
Terrain roughness length z ₀ [6.3.2, A.3, A.4]	Net wind pressure p _{net} [7.3(1)]	$h/\sqrt{(b\cdot d)}$ < 3: not relevant
Neighbouring construction works [A.5]	Relevance of wind friction [7.4(2)]	$3 \le h/\sqrt{(b \cdot d)} \le 6 \text{ [F.3]}$
Displacement height h _{dis} [A.6]	Friction coefficient c_{fr} [D.9]	Transverse resonance turbulence effect [Annex F]
Significance of orography: $\Phi = H/L_u > 5 \% [6.3.3, A.4]$	Forces from friction F_{tr} [Formula (7.9)]	$6 < h/\sqrt{(b \cdot d)} \le 8 \text{ [F.3]}$
Not significant: c _o =1 [A.4]	Resulting wind force $F_{wse}[7.6(1)]$	Most onerous should be used [Annex F-G]
Significant: c_o [A.4] 3. Specific wind velocity and velocity pressure	Forces from wind pressure, friction and force coefficients [Formulas (7.4, 7.6-7.8)]	$h/\sqrt{(b\cdot d)} > 8 \text{ [F.3]}$
Fluctuating wind components	b) Bridges and other line-like structures	Vortex induced vibrations [9.3, Annex G]
Structural height h ≤ 200m	Reference height z _c [Annex D]	Galloping [9.4, Annex G]
Roughness factor c_r [Formula (6.6)]	Force coefficient c_f [Annex D]	Divergence and Flutter [9.5, Annex G]
Turbulence intensity I _u [Formula (6.10)]	Wind force F_{wse} [Formula (7.9)]	Wake buffeting [9.6]
Structural height 200m <h≤ 300m="" [a.7]<="" th=""><th>Additional rules for lattice towers guyed masts [Annex I]</th><th>Other flexible structures (chimneys, bridges decks etc.)</th></h≤>	Additional rules for lattice towers guyed masts [Annex I]	Other flexible structures (chimneys, bridges decks etc.)
Roughness factor c _r [A.7.2] Turbulence Intensity I _n [A.7.3]	c) Other structures (e.g. freestanding walls, roofs and signboards)	Vortex induced vibrations [9.3, Annex G]
Mean wind velocity v _m [Formula (6.4)]	Reference height $z_{\rm e}$ [Annex C]	Galloping [9.4, Annex H]
Peak wind velocity v_p [Formula (6.11)]	Net pressure coefficient $c_{p,met}$ [Annex C]	Divergence and Flutter [9.5, Annex G]
Peak velocity pressure q_p [Formula (6.12)]	Net wind pressure p_{net} [7.3(1)]	Wake buffeting [9.6]
	Net wind force F_{pact} [Formula (7.6)]	
	Forces from friction F_{fr} [D.9]	

Figure 5.1 — Overview of the general design process and classification regarding the relevance of methods for individual design situations



EN 1991-1-5 Thermal

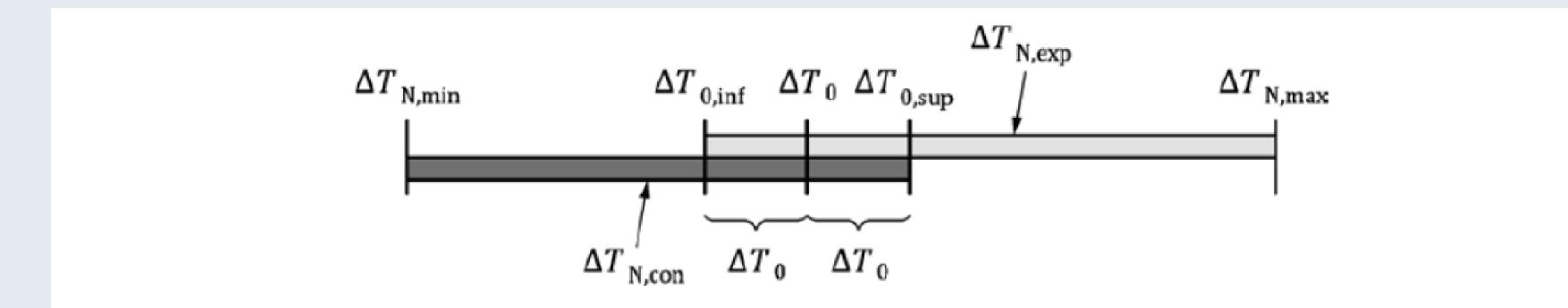
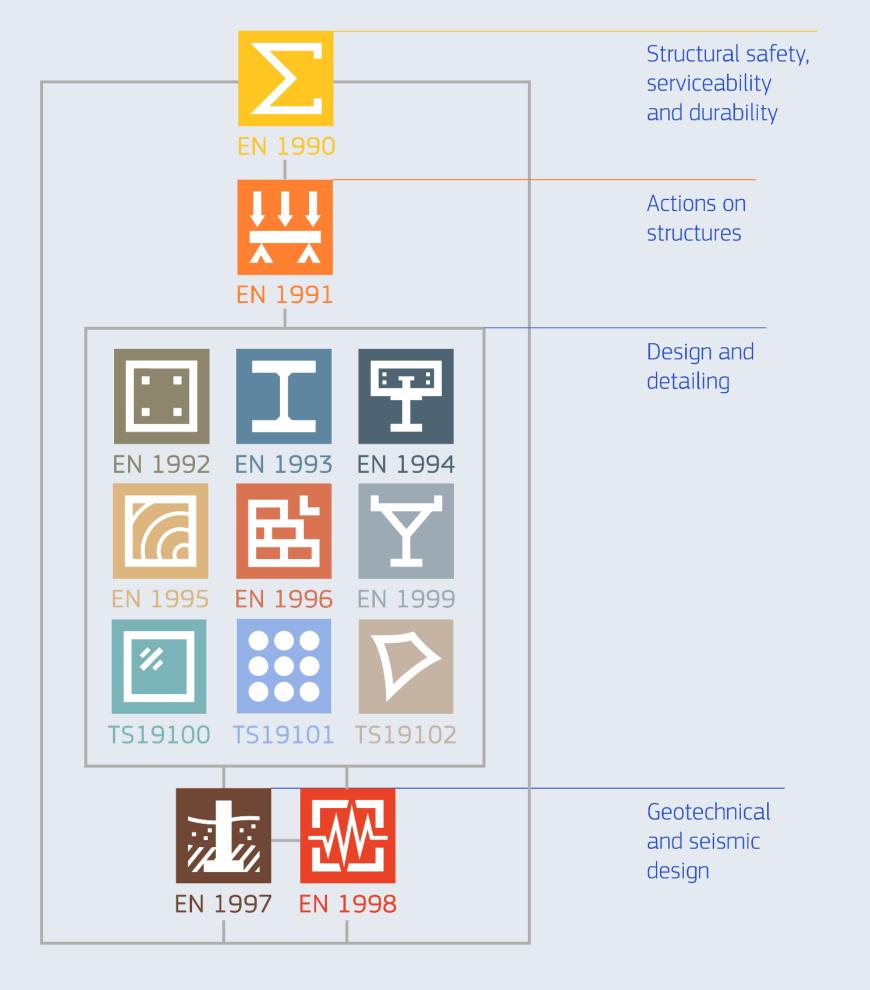


Figure 8.1 — Characteristic value of the maximum contraction ($\Delta T_{N,\text{con}}$) and expansion ($\Delta T_{N,\text{exp}}$) range of the uniform bridge temperature component



Eurocode Second Generation Updates EN 1990 Basis of Design and EN 1991 Actions on Structures





THE FUTURE OF STEEL CONSTRUCTION

30 March 2028

Thank you